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Using the $6 \mathrm{~ms} / \mathrm{m}$ curve, the estimated radius of the $0.5 \mathrm{mV} / \mathrm{m}$ contour is 62.5 kilometers. Subtracting this distance from the distance between the two stations leaves 197.5 kilometers. Using the same propagation curve, the signal from the 5 kW station at this distance is seen to be $0.059 \mathrm{mV} / \mathrm{m}$. Since a protection ratio of 6 dB , desired to undesired signal, applies to stations separated by 10 kHz , the undesired signal could have had a value of up to $0.25 \mathrm{mV} / \mathrm{m}$ without causing objectionable interference. For cochannel studies, a desired to undesired signal ratio of no less than $20: 1(26 \mathrm{~dB})$ is required to avoid causing objectionable interference.
(d) Where a signal traverses a path over which different conductivities exist, the distance to a particular groundwave field strength contour shall be determined by the use of the equivalent distance method. Reasonably accurate results may be expected in determining field strengths at a distance from the antenna by application of the equivalent distance method when the unattenuated field of the antenna, the various ground conductivities and the location of discontinuities are known. This method considers a wave to be propagated across a given conductivity according to the curve for a homogeneous earth of that conductivity. When the wave crosses from a region of one conductivity into a region of a second conductivity, the equivalent distance of the receiving point from the transmitter changes abruptly but the field strength does not. From a point just inside the second region the transmitter appears to be at that distance where, on the curve for a homogeneous earth of the second conductivity, the field strength equals the value that occurred just across the boundary in the first region. Thus the equivalent distance from the receiving point to the transmitter may be either greater or less than the actual distance. An imaginary transmitter is considered to exist at that equivalent distance. This technique is not intended to be used as a means of evaluating unattenuated field or ground conductivity by the analysis of measured data. The method to be employed for such determinations is set out in §73.186.
(e) Example of the use of the equivalent distance method;

It is desired to determine the distance to the $0.5 \mathrm{mV} / \mathrm{m}$ and $0.025 \mathrm{mV} / \mathrm{m}$ contours of a station on a frequency of 1000 kHz with an inverse distance field of $100 \mathrm{mV} / \mathrm{m}$ at one kilometer being radiated over a path having a conductivity of $10 \mathrm{mS} / \mathrm{m}$ for a distance of 20 kilometers, $5 \mathrm{mS} / \mathrm{m}$ for the next 30 kilometers and $15 \mathrm{mS} / \mathrm{m}$ thereafter. Using the appropriate curve in $\S 73.184$, Graph 12, at a distance of 20 kilometers on the curve for 10 $\mathrm{mS} / \mathrm{m}$, the field strength is found to be 2.84 $\mathrm{mV} / \mathrm{m}$. On the $5 \mathrm{~ms} / \mathrm{m}$ curve, the equivalent distance to this field strength is 14.92 kilometers, which is 5.08 ( $20-14.92$ kilometers nearer to the transmitter. Continuing on the propagation curve, the distance to a field strength of $0.5 \mathrm{mV} / \mathrm{m}$ is found to be 36.11 kilometers.
The actual length of the path travelled, however, is 41.19 ( $36.11+5.08$ ) kilometers. Continuing on this propagation curve to the conductivity change at 44.92 (50.00-5.08) kilometers, the field strength is found to be 0.304 $\mathrm{mV} / \mathrm{m}$. On the $15 \mathrm{mS} / \mathrm{m}$ propagation curve, the equivalent distance to this field strength is 82.94 kilometers, which changes the effective path length by 38.02 ( $82.94-44.92$ ) kilometers. Continuing on this propagation curve, the distance to a field strength of 0.025 $\mathrm{mV} / \mathrm{m}$ is seen to be 224.4 kilometers. The actual length of the path travelled, however, is 191.46 (224.4+5.08-38.02) kilometers.
[28 FR 13574, Dec. 14, 1963, as amended at 44 FR 36037, June 20, 1979; 48 FR 9011, Mar. 3, 1983; 50 FR 18822, May 2, 1985; 50 FR 24522, June 11, 1985; 51 FR 9965, Mar. 24, 1986; 54 FR 39736, Sept. 28, 1989; 56 FR 64866, Dec. 12, 1991; 57 FR 43290, Sept. 18, 1992]

## §73.184 Groundwave field strength graphs.

(a) Graphs 1 to 20 show, for each of 20 frequencies, the computed values of groundwave field strength as a function of groundwave conductivity and distance from the source of radiation. The groundwave field strength is considered to be that part of the vertical component of the electric field which has not been reflected from the ionosphere nor from the troposphere. These 20 families of curves are plotted on log-log graph paper and each is to be used for the range of frequencies shown thereon. Computations are based on a dielectric constant of the ground (referred to air as unity) equal to 15 for land and 80 for sea water and for the ground conductivities (expressed in $\mathrm{mS} / \mathrm{m}$ ) given on the curves. The curves show the variation of the groundwave field strength with distance to be expected for transmission from a vertical
antenna at the surface of a uniformly conducting spherical earth with the groundwave constants shown on the curves. The curves are for an antenna power of such efficiency and current distribution that the inverse distance (unattenuated) field is $100 \mathrm{mV} / \mathrm{m}$ at 1 kilometer. The curves are valid for distances that are large compared to the dimensions of the antenna for other than short vertical antennas.
(b) The inverse distance field ( $100 \mathrm{mV} /$ $m$ divided by the distance in kilometers) corresponds to the groundwave field intensity to be expected from an antenna with the same radiation efficiency when it is located over a perfectly conducting earth. To determine the value of the groundwave field intensity corresponding to a value of inverse distance field other than $100 \mathrm{mV} /$ $m$ at 1 kilometer, multiply the field strength as given on these graphs by the desired value of inverse distance field at 1 kilometer divided by 100; for example, to determine the groundwave field strength for a station with an inverse distance field of $2700 \mathrm{mV} / \mathrm{m}$ at 1 kilometer, simply multiply the values given on the charts by 27 . The value of the inverse distance field to be used for a particular antenna depends upon the power input to the antenna, the nature of the ground in the neighborhood of the antenna, and the geometry of the antenna. For methods of calculating the interrelations between these variables and the inverse distance field, see "The Propagation of Radio Waves Over the Surface of the Earth and in the Upper Atmosphere,', Part II, by Mr. K.A. Norton, Proc. I.R.E., Vol. 25, September 1937, pp. 1203-1237.

Note: The computed values of field strength versus distance used to plot Graphs 1 to 20 are available in tabular form. For information on obtaining copies of these tabulations call or write the Consumer Affairs Office, Federal Communications Commission, Washington, DC 20554, (202) 632-7000.
(c) Provided the value of the dielectric constant is near 15 , the ground conductivity curves of Graphs 1 to 20 may be compared with actual field strength measurement data to determine the appropriate values of the ground conductivity and the inverse distance field strength at 1 kilometer. This is accomplished by plotting the
measured field strengths on transparent log-log graph paper similar to that used for Graphs 1 to 20 and superimposing the plotted graph over the Graph corresponding to the frequency of the station measured. The plotted graph is then shifted vertically until the plotted measurement data is best aligned with one of the conductivity curves on the Graph; the intersection of the inverse distance line on the Graph with the 1 kilometer abscissa on the plotted graph determines the inverse distance field strength at 1 kilometer. For other values of dielectric constant, the following procedure may be used to determine the dielectric constant of the ground, the ground conductivity and the inverse distance field strength at 1 kilometer. Graph 21 gives the relative values of groundwave field strength over a plane earth as a function of the numerical distance $p$ and phase angle $b$. On graph paper with coordinates similar to those of Graph 21, plot the measured values of field strength as ordinates versus the corresponding distances from the antenna in kilometers as abscissae. The data should be plotted only for distances greater than one wavelength (or, when this is greater, five times the vertical height of the antenna in the case of a nondirectional antenna or 10 times the spacing between the elements of a directional antenna) and for distances less than $80 \mathrm{f}^{1 / 3} \mathrm{MHz}$ kilometers (i.e., 80 kilometers at 1 MHz ). Then, using a light box, place the plotted graph over Graph 21 and shift the plotted graph vertically and horizontally (making sure that the vertical lines on both sheets are parallel) until the best fit with the data is obtained with one of the curves on Graph 21. When the two sheets are properly lined up, the value of the field strength corresponding to the intersection of the inverse distance line of Graph 21 with the 1 kilometer abscissa on the data sheet is the inverse distance field strength at 1 kilometer, and the values of the numerical distance at 1 kilometer, $p_{1}$, and of $b$ are also determined. Knowing the values of $b$ and $p_{1}$ (the numerical distance at one kilometer), we may substitute in the following approximate values of the ground conductivity and dielectric constant.

$$
\begin{equation*}
\mathrm{x} \cong \frac{\pi}{p} \cdot\left(\frac{\mathrm{R}}{\lambda}\right)_{1} \cdot \cos b \tag{Eq.1}
\end{equation*}
$$

$(R / \lambda)_{1}=$ Number of wavelengths in 1 kilometer,
$\mathrm{f}_{\mathrm{MHz}}=$ frequency expressed in megahertz,

$$
\begin{equation*}
\varepsilon \cong \chi \tan b-1 \tag{Eq.3}
\end{equation*}
$$

$\varepsilon=$ dielectric constant on the ground referred to air as unity.
First solve for $\chi$ by substituting the known values of $p_{1},(\mathrm{R} / \lambda)_{1}$, and $\cos b$ in equation (1). Equation (2) may then be solved for $\delta$ and equation (3) for $\varepsilon$. At distances greater than $80 / \mathrm{f}^{1 / 3} \mathrm{MHz}$ kilometers the curves of Graph 21 do not give the correct relative values of field strength since the curvature of the earth weakens the field more rapidly than these plane earth curves would indicate. Thus, no attempt should be made to fit experimental data to these curves at the larger distances.

Note: For other values of dielectric constant, use can be made of the computer program which was employed by the FCC in generating the curves in Graphs 1 to 20. For information on obtaining a printout of this program, call or write the Consumer Affairs Office, Federal Communications Commission, Washington, DC 200554, (202) 632-7000.
(d) At sufficiently short distances (less than 55 kilometers at AM broadcast frequencies), such that the curvature of the earth does not introduce an additional attenuation of the waves, the curves of Graph 21 may be used to determine the groundwave field strength of transmitting and receiving antennas at the surface of the earth for any radiated power, frequency, or set of ground constants. First, trace the straight inverse distance line corresponding to the power radiated on transparent log-log graph paper similar to that of Graph 21, labelling the ordinates of the chart in terms of field strength, and the abscissae in terms of distance. Next, using the formulas given on Graph 21, calculate the value of the numerical distance, $p$, at 1 kilometer, and the value of $b$. Then superimpose the log-log graph paper over Graph 21, shifting it vertically until both inverse distance lines coincide
and shifting it horizontally until the numerical distance at 1 kilometer on Graph 21 coincides with 1 kilometer on the log-log graph paper. The curve of Graph 21 corresponding to the calculated value of $b$ is then traced on the log-log graph paper giving the field strength versus distance in kilometers.
(e) This paragraph consists of the following Graphs 1 to 20 and 21.
Note: The referenced graphs are not published in the CFR, nor will they be included in the Commission's automated rules system. For information on obtaining copies of the graphs call or write the Consumer Affairs Office, Federal Communications Commission, Washington, DC 20554, Telephone: (202) 632-7000.
[28 FR 13574, Dec. 14, 1963, as amended at 50 FR 18823, May 2, 1985; 51 FR 45891, Dec. 23, 1986; 52 FR 36878, Oct. 1, 1987; 56 FR 64866, Dec. 12, 1991; 57 FR 43290, Sept. 18, 1992]

## § 73.185 Computation of interfering signal.

(a) Measured values of radiation are not to be used in calculating overlap, interference, and coverage.
(1) In the case of an antenna which is intended to be non-directional in the horizontal plane, an ideal non-directional radiation pattern shall be used in determining interference, overlap, and coverage, even if the antenna is not actually non-directional.
(2) In the case of an antenna which is directional in the horizontal plane, the radiation which shall be used in determining interference, overlap, and coverage is that calculated pursuant to $\S 73.150$ or $\S 73.152$, depending on whether the station has a standard or modified standard pattern.
(3) In the case of calculation of interference or overlap to (not from) a foreign station, the notified radiation shall be used, even if the notified radiation differs from that in paragraphs (a) (1) or (2) of this section.
(b) For skywave signals from stations operating on all channels, interference shall be determined from the appropriate formulas and Figure 6 a contained in §73.190.
(c) The formulas in $\S 73.190(\mathrm{~d})$ depicted in Figure 6a of $\S 73.190$, entitled "Angles of Departure versus Transmission Range" are to be used in determining the angles in the vertical pattern of the antenna of an interfering

